HENLEY BROOK AVENUE EXTENSION

REVEGETATION MANAGEMENT PLAN

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1 INTRODUCTION

1.1 Background

The City of Swan is in the process of planning for the extension of Henley Brook Avenue from its current alignment near Gnangara Road to south of Henley Street (Figure 1). The proposed road works will be partly within an unmade road reserve at the northern end and through mostly private lots at the southern end (Figure 2).

The road works will result in the clearing of approximately 2.0ha of native vegetation, of which 0.64ha is foraging habitat for Black Cockatoos. An application for a Clearing permit was originally submitted to the Department of Water and Environmental Regulation (DWER) (CPS 9953/1) for the entire road to be constructed, however the northern part of the reserve does not contain any significant vegetation so was split from the southern part. The northern part was granted a clearing permit approval on 26 July 2023. The southern part is the subject of a new application. During discussions DWER indicated that a Revegetation Management Plan (RMP) should accompany the application for the southern part of the road works.

PGV Environmental was commissioned by the City of Swan to prepare a Revegetation Management Plan (RMP) to be implemented to manage the impact of the proposed road works.

1.2 Location of Revegetation

The proposed revegetation will be undertaken in the Henley Brook Avenue Road Reserve upon the completion of the construction of the road. The parts of the road reserve that are proposed for revegetation include the median strips and central parts of the roundabouts, and around the drainage basin. The revegetation works include the southern portion that is subject to a new clearing permit as well as the northern portion which received a clearing permit on 26 July 2023.

1.3 Purpose

Planting of trees in the constructed Henley Brook Avenue road reserve is being undertaken for the purpose of offsetting the impact of clearing Black Cockatoo foraging and potential breeding habitat in association with the road works. The RMP has been prepared to set out the strategies for the design, implementation, monitoring and maintenance activities of revegetation works.

1.4 Objective

The overall objective of the RMP is to re-establish Black Cockatoo foraging and potential breeding habitat in the Henley Brook Avenue Road reserve. The final planting will result in a net gain of habitat within the road reserve.

1.5 Scope of Work

The RMP has been prepared in accordance with DWER's *Guide to Preparing Revegetation Plans for Clearing Permits* and includes the following:



- A description of the area to be revegetated within the road reserve;
- Revegetation commitments;
- Site preparation;
- Species list compilation and revegetation techniques;
- Monitoring and analysis;
- Schedule of Works;
- Targets and completion criteria; and
- Maintenance and contingency measures.

1.6 Legislation and Regulatory Framework

Legislation directly relevant to the management of native vegetation in Western Australia and to this RMP is provided in Table 2.

Legislation	Application
Biodiversity Conservation Act (WA) 2016 (BC Act)	Conservation and protection of biodiversity and biodiversity components. This Act repeals the <i>Wildlife Conservation Act 1950.</i>
Environment Protection Act 1986 (WA) (EP Act)	Prevention, control and abatement or pollution and conservation protection and enhancement of environment. Application for the Clearing Permit is made under S38.
Environmental Protection (Clearing of Native Vegetation) Regulations 2004 (WA)	Regulates the clearing of native vegetation.
Rights in Water and Irrigation Act 1914 (WA) (RIWI Act)	Relates to rights in water resources, to make provisions for the regulation, management, use and protection of water resources, to provide for irrigation schemes and for related purposes. Applies to works around St Leonard's Creek.

Table 1: Relevant Legislation



2 EXISTING ENVIRONMENT

2.1 Climate and Rainfall

Western Australia experiences a Mediterranean climate with warm dry summers and wet cool winters. Peak rainfall periods are between May and September. Climate statistics from the Bureau of Meteorology (BOM, 2023) provide mean values for maximum and minimum temperature and rainfall (Graph 1). The statistics have been measured on the Perth Aero Site (BOM Site Number 009021), which has been collecting data from 1951.



Graph 1: Mean Climate Statistics

2.2 Topography

The site is mostly flat 30-32 m Australian Height Datum (AHD) with a ridge line at the northern end rising up to 40m AHD (Figure 2).

2.3 Geology and Soils

The site is mapped on the Bassendean Dune System and consists of very low relief, leached, grey siliceous Pleistocene sand dunes, intervening sandy and clayey swamps and gently undulating plains (Bolland, 1998). These soils are very leached, infertile and mildly acidic (DPIRD, 2023).

The soil phases mapped on the site are:

 Bassendean, Jandakot Phase (212Bs_Ja) which is associated with low, gently sloping dunes on Aeolian sands. The soils are described as grey sand over pale yellow sands generally underlain by humic and iron podzols;



- Bassendean Yanga Phase (Bassendean) Phase (212Bs_Ya) which are located on poorly drained flats on alluvial deposits. The soils are semi-wet soils, yellow-brown shallow sands and grey deep sandy duplexes and are usually associated with dense *Melaleuca* scrub; and
- Bassendean Joel Phase (212Bs_J) which are poorly drained depressions with humus podzols; and
- VC Valley complex (Bassendean) (212Bs_VC) which are variable soils associated with drainage lines associated with St Leonards Creek (DPIRD, 2023).

2.4 Hydrology

2.4.1 Groundwater

The site is on the Perth Surficial Swan and Mirrabooka aquifer. The Superficial Swan overlays the Leederville aquifer which is further described as the sub area Wanneroo member under the site and consists of poorly sorted fine – to medium-grained quartz with feldspar and occasionally trace heavy minerals. This overlays the Yarragadee aquifer (DoW, 2015).

Groundwater flows generally to the south-east and is between 27mAHD and 30mAHD (DWER, 2023). The depth to groundwater from the natural surface ranges from approximately 3 to 5m (DoW, 2015b). Annual average maximum water levels will be higher than the May 2003 levels as indicated.

2.4.2 Surface Water

The southern end of the road extension works site passes through a 'Multiple Use' palusplain wetland (UFI 13396) (shown in blue on Plate 1). The wetland in this location is highly modified and largely cleared of native vegetation.



Plate 1: Wetland Mapping (National Map, 2023)



The southern part of the extension crosses over a portion of the northern arm of St Leonards Creek. In this location the creek has been highly modified into a drain. The aerial photograph from 1965 (Landgate, 2023) shows the creekline has been excavated (Plate 2), most likely to facilitate draining of the Multiple Use palusplain wetland.





2.5 Vegetation

2.5.1 Vegetation Description

The vegetation on the site is a mixture of planted trees such as River Red Gums (*Eucalyptus camaldulensis*) and Tuart (*Eucalyptus gomphocephala*) and scattered remnant native Jarrah (*Eucalyptus marginata*), Banksia (*Banksia attenuata*, *B. menziesii*) and Marri (*Corymbia calophylla*). Most of the Marri trees are young (Plate 8), however several larger trees also occur.

A stand of *Acacia saligna* (Orange Wattle) shrubs and *Adenanthos cygnorum* (Woolly Bush) occur in the central part of the site.

The northern part of the road works contains only 0.043ha of scattered native vegetation and otherwise contains non-native Geraldton Wax, weeds or bare ground.

2.5.2 Vegetation Condition

The vegetation condition of the road reserve is Completely Degraded according to the condition scale of Keighery (1994) published in Bush Forever (Government of Western Australia, 2000).



3 REVEGETATION MANAGEMENT PLAN

3.1 Revegetation Context

The proposed revegetation in the road reserve will be the planting of trees in landscaped areas rather than the re-creation of intact native trees and understorey. The landscaping will consist of a tree canopy over mulch due to insufficient water allocation for the installation of a reticulation system for smaller shrubs. The canopy will provide habitat for Black Cockatoos, similar to the current habitat, with Eucalypt/Corymbia and Banksia trees.

The drainage basin located near St Leonards Creek Landscaping in the drainage basin will be landscaped with largely native species. The basin will be planted with a mixed of reeds to trap any sediments and utilise any nutrient run-off from the road. The upper banks and top will be planted with an overstorey consistent with the species utilised for the median strips.

The revegetation will result in the planting of at least 44 trees being established within the road reserve and a net gain in foraging habitat. (replacing potential breeding habitat at a ratio of 3.4:1) The revegetation will establish a canopy in the northern part of the road extension that is currently non-existent.

3.2 Site Preparation

The site will be completely cleared and median strips established as per standard road construction. The soil within the median strip will be stabilised with mulch prior to planting.

3.3 Species

The proposed revegetation will consist of tree species that will be procured as more mature specimens in 45 to 100L pots. The native species recommended for use (Table 2) have been selected using four criteria as follows:

- 1. The species will be consistent with other sections of the constructed road;
- 2. The species are known Black Cockatoo foraging and potential breeding habitat species;
- 3. The species used will be able to tolerate the site conditions without the requirement for water; and
- 4. The species should be available from plant nurseries.

Table 2: Native Species for Rehabilitation

Species	Common Name	Foraging habitat	Potential Breeding Habitat
Banksia prionotes	Acorn Banksia	✓	
Callistemon viminalis/King's Park Special	Bottle Brush		
Corymbia calophylla	Marri	~	~
Eucalyptus accedens	Powderbark Wandoo		~
Eucalyptus marginata	Jarrah	✓	~
Eucalyptus todtiana	Black Butt	~	
Hakea laurina	Pincushions	×	



The drainage basin will be planted with native vegetation to encourage biological nutrient uptake, consistent with the *Vegetation guidelines for stormwater biofilters in the south-west of Western Australia* (Monash University, 2014). The species chosen will have extensive and fine root systems, be relatively fast growing, be able to withstand temporary and regular inundation, and have long growing seasons. A sufficient density of plants of at least 4/m2 is recommended to provide adequate initial coverage and room for growth. Species will be native and planting in accordance with WQPN 84: Rehabilitation of disturbed land in PDWSAs (DWER, 2009).

3.4 Planting

Species will be planted in rows within the median strip and in the central part of roundabouts. Infill planting will be undertaken if any areas do not meet the completion criteria after 1 year.

3.5 Weeding

Weeds will be minimal in the median strip as the soil will be stripped from the site during roadworks. Revegetation of road reserve median strips will commence at the first break of season where any weeds that have subsequently grown on the site will be sprayed or removed by hand by an appropriately qualified weed contractor using methodology guided by the species profile in Florabase (https://florabase.dpaw.wa.gov.au/) (DBCA, 2023).

3.6 Completion Criteria

The following targets will be used to assess the performance of the rehabilitation and identify if additional seeding/planting or management works are required:

- Survival of 80% of trees planted in the median strip and in the central areas of the roundabouts;
- A maximum weed cover of 5%; and
- No bulbous weeds, Declared Pests (such as Pampas grass, Bridal Creeper, Cape Tulip, Narrow-Leaf Cotton Bush, Paterson's Curse, Caltrop), noxious weeds, or woody weeds within the revegetated area.

3.7 Monitoring

Monitoring of the revegetation will be a visual inspection of all planted trees within the median strip and in the roundabouts.

Monitoring of the revegetation area will commence in October/November following planting to establish initial survival rates and a follow-up in March/April the following year to monitor the survival rate over summer. Monitoring will continue annually in October/November and March/April each subsequent year until the completion criteria have been reached for a period of at least three years.

3.8 Weed Management

Post planting weed control will be undertaken for a minimum of 2 years post planting and be undertaken twice a year to ensure weeds do not dominate the site. Management measures will be guided by monitoring result to identify the weeds present. Appropriate management techniques as



per the species profile in Florabase (<u>https://florabase.dpaw.wa.gov.au/</u>) (DBCA, 2023) will be utilised to manage any emergent weeds on the site.

If weed species are considered likely to pose a threat to achieving successful revegetation results, then weed control appropriate to the species will be undertaken. Weed management will be effective for two years after initial planting.

3.9 Timing

Planting will take place after earthworks for the road batters and roundabouts have been completed and mulched. Planting will commence after opening rains of 100mm in the autumn/winter period which generally is in June/July, consistent with *Guide to Preparing Revegetation Plans for Clearing Permits*. Table 3 outlines the proposed timing for revegetation works.

Year	Time	Phase	Pest/Weed Control	Planting	Monitoring
	Commencement	Soil pile to be removed	Not required – all weeds will be removed with soil		
1	Winter	Planting commences		After 100mm of rain has fallen (break of season)	
	Spring		Spray September to October if required		Monitoring commences
	Summer				Monitoring
	Autumn	Infill Planting	Spray in April to May if required		Monitoring
2	Winter			Break of season	Monitoring
2	Spring		Spray September to October if required		Monitoring
	Summer				Monitoring
		If survival com	pletion criteria not met	repeat Year 2	
	Autumn		Spray in April to May if required		Monitoring
2	Winter	Maintenance			Monitoring
3	Spring	Year 1	Spray September to October if required		Monitoring
	Summer				Monitoring
	Autumn		Spray in April to May if required		Monitoring
4	Winter	Maintenance			Monitoring
4	Spring	Year 2	Spray September to October if required		Monitoring
	Summer				Monitoring
		Co	mpletion if criteria are m	et	

Table 3: Timing for Revegetation Works



3.10 Contingencies

If the completion criteria are not likely to be met after the first two monitoring periods, then further planting will occur in the second year using the species from Table.

If there is a significant decline or loss in surviving plants the following contingency plan will be implemented:

- 1. Determine if the decline may be within normal limits ie due to harsh summer conditions.
- 2. Consider potential causes for decline in vegetation health including but not limited to:
 - a. Increase in competition with weed species;
 - b. Predation by herbivores including rabbits and possibly kangaroos; or
 - c. Water stress.
- 3. Implement measures to manage identified causes which may include, but not limited to:
 - a. Management of weed species;
 - b. Use of tree guards; or
 - c. Watering during summer months.
- 4. Infill plants into impacted areas in the next planting season to ensure that the completion criteria can be met.
- 5. Continue monitoring vegetation health and the effectiveness of remedial actions.

3.11 Reporting

A letter report addressing compliance with this management plan and results of the monitoring to demonstrate meeting the completion criteria will be prepared and retained as part of the records keeping required for the Clearing Permit after the completion criteria have been met.



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FIGURES



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APPENDIX 1

Drainage Design







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		AL1 SEP AM1 HW Deuble	65506.05 279240.31 65493.63 279181.58	11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Direct Kinematic Wave	597.18 0.4	0.25 296.87 10.01	0.4 19.6082 7.44	15 0.0505 16.5 13 7.4433 207	0.0505 0.0505 16.5 16.5 16.5 14.433 7.44.33 2.07 2.07	16.9	482.9 0.049 1.7	0.(2 0.5 3	-	56,30X 16.5 0.4 207	AKI		
		AM2 HW autlet Dauble	65525.35 279166.53	30.17 30.95 30.95	0		2744	00 0000	1 0.050 H	0.0044 0.00544 44.° 44.7	64	0100 0001	c 30 670		50 031 AC	-		
		A01 GULLY	65467.16 278839.28	35.83 35.83 35.83 1	Direct		5 117.65	E0.0 6EE0.0 6.0	15 11.8964 14.20.2	0.0305 1.874.8 612.7 14.20.2	1420.2	1579.1 0.14.6 5.9	0.16 3.2 1		16,0.5X 74 134.6.2	LOST		
		A02 SEP	65482.53 278859.15	36.03 36.03 36.03 1	Direct	C.7 0.01	0.25 32.11 44.20 5 117.65	0.4 29.0040 11.01	7.61 60.0663 19.7	0.0603 0.0603 19.7 19.7	1.61	14.75.2 0.032 1.74	0.(2 2.7 15	-	2G,15X 13.9 5.8	AZ1		
		A03 SEP A04 MH	65495.39 278874.71 65496.55 278950.97	35.87 35.87 35.87 11 33.78 33.78 33.78	Direct		5 117.65	0.9 0.0151 0.01	5'7 9EL0'0 9E	0.0136 0.0136 4.5 4.5	4.5	3048.7 0.014 1.5	1 9.6 11.0	-	4G,0.5X 3.6 0.9			
		ADS SEPTWIN ADS CED	65507.66 278964.22 6550937 279000.2	11 33.16 33.16 33.16 11 33.16 11 33.16 11 33.16 11 33.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.16 13.	Direct		5 117.65 5 117.65	0.9 0.14.11 0.12	7 0.127 415	0.127 0.127 4.15 4.15	415	553.5 0.056 19 321.6 0.059 2.0	0.04 15 3		20,30X 29.6 119 56.30X 23 36	A06 A07		
		A07 SEP	65512.51 279039.32	32.62 32.62 1	Direct		5 117.65	70'0 7ESO'0 6'0	12:51 1870.0 18	1.51 1.51 1.870'0 1.870'0	7.61	321.6 0.052 1.8	0.(2 0.5		56,3.0X 18.5 0.9	A08		
		A03 SEP A09 SEP	65514.42 279119.16 65517.66 279119.16	32.46 32.46 32.46 1 32.23 32.23 32.23 1	Direct		5 117.65	0.0 9700 0.04	32 0.0432 14.1	0.0432 0.0432 14.2 14.1 0.0414 0.0414 13.5 13.5	15	321.6 0.048 161 321.6 0.046 1.6	0.02 0.5 3		56,3.0X 15 56,3.0X 13.5	A010		
		A010 SEP A011 SEP	65520.4.4 279159.06 65523.22 279198.96	32.04 32.04 32.04 11 31.85 31.85 31.85 11	Direct		5 117.65 5 117.65	0.9 0.0466 0.04	22 0.0422 13.8 2 0.042 13.7	0.0422 0.0422 13.6 13.8 0.042 0.042 13.7 13.7	13.8	321.6 0.046 16 321.6 0.046 1.6	0.(2 0.5 3		56,30X 138 56,30X 13.7	A011 A012		
		A012 SEP 2012 SEP	65526 279238.87	31.66 31.66 31.66 1	Direct		5 117.65	0.9 0.0455 0.04	1 0.041 13.4	0.041 0.041 13.4 13.4	13.4	321.6 0.046 1.5	0.(2 0.5 3		56,3.0X 13.4	A013		
		A015 2EP A014 SEP	6553156 279318.67	11 03140 31.40 31.40 11 31.27 31.27 31.27 11	Direct		5 117.65 5 117.65	20.0 61.00 0.03 0.0 0.0433 0.03	9 0.039 12.7	0.0377 0.0377 12: 12:3	12.3	283.5 0.047 1.6	0.(2 0.5 3		56,30X 12.3 56,30X 12.7	A015		
		A015 COMB0 SEP TWIN A016 HW sufflet	65533.97 279353.34	31.2 31.2 31.2 1 29.7 31.2 31.2 1	Direct		5 117.65	0.9 0.0812 0.07	31 0.0731 23.9	0.0731 0.0731 23.9 23.9	23.9	36.8 0.036		0.04.5 1	23.9	1 0		
		AP1 SEP AQ1 SEP	55497.7 279120.4 55494.47 279074.03	32.24 32.24 32.24 1 32.47 32.47 1	Direct		5 117.65 5 117.65	0.9 0.0568 0.05	11 0.0511 16.7 5 0.0515 16.8	0.0511 0.0511 16.1 16.7 0.0515 0.0515 16.4 16.8	18.1	482.9 0.05 1.8 482.9 0.053 1.9	0.(2 0.5 3		56,30X 17.5 0.6 56,30X 19.6 1.4	AN1 AP1		
		ARI GULLY	654.97.64 278862.01	36.37 36.37 36.37 1	Direct		5 117.65	0.9 0.0177 0.01	(9 0.0159 5.2	0.0159 0.0159 5.2 5.2	5.2	1158.9 0.02 3.8	0 11 39 2	-	46,15X 5.1 0.1	A03		
		AS2 GULLY	65502.03 278789.94	35.36 35.36 35.36 1	Direct		5 117.65	0.9 0.0653 0.05	18 0.0588 19.2	0.0588 0.0588 19.2 19.2	19.2	7073.4 0.035 1.24	0.03 3.9 2.1	-	46,15X 13.7 5.5	AS3		
		AS3 SEP AS4 SEP	65541.567 27874.2.79 65541.56 278694.49	33.44 33.44 31.44 11 31.44 31.44 31.44 11	Direct		5 117.65 5 117.65	0.9 0.0819 0.07	9 0.0737 24.1	0.0737 0.0737 24.1 24.1 0.0739 0.0739 24.1	35.9	1278 0.041 14 2594.8 0.034 2.7	0.04 3.7 3		26,15X 17.9 11.8 26,15X 18.8 17.1	AS6 AS6		
		AS5 MH AS6 SEP	65555.9 278689.43 65579.52 278646.89	31.3 31.3 31.3 29.81 29.81 29.81 1	Direct		5 117.65	580.0 6560.0 5.0	9 0.0859 29.4	3.0899 0.0899 29.4 29.4	46.5	633.5 0.055 1.9;	0.05 2.1 3	-	2G,3 0X 26 20.6			
		AS7 GULY TWIN AT1 KEP	65602.37 278644.4 645434.28 278827.3	28.76 28.76 28.76 27.6 37.6 37.6							c		56	-	26.15X 0			
		AT2 GULLY AM1 CFD	65514.31 278802.33 65514.78 278567.67	36.21 36.21 36.21 11 29.05 29.05 29.05 11	Direct		5 117.65 6 117.65	0.9 0.103 0.09	0.0527 30.3 8 32 9005 1	E.0E 5027 0.0927 30.2 80.7 80.7	30.3	0.4 0.005 1.7	0.0 4.2 21		46,15X 20.1 10.2 56.3 nV 105 94.8 5	LOST		
		2m2	2222050	30 12 20 12 30 15 30 15	> Kinematic Wave	624.5 0.6	0.25 247.65 11.27	0.4 82.2567 32.91	27	E1999.0								
		AZI SEPTWIN	65485.95 278951.69	33.37 33.37 33.37 11	Direct		5 117.65	0.9 0.1607 0.14	E.74 74410 T.	0.1447 0.1447 47.3 47.3	53.1	945.1 0.058 2.1	0.05 2 3	-	2G,3.0X 34.2 18.9	801		
		BI SEPTIMIN BBI COMBO SEP	654.08.88 280240.86	35.43 35.43 35.43 1	Direct		cerrit c	0.9 0.1226 0.110	3 0.1103 36	0.1103 0.1103 36 36	2772	7/1 C0/0 1/9189 7/2 5809/6 0.069	0.05 0.9 3	0.61	16,3.0X 215 33.2	12		
		BB2 MH BC1 SEP	65409.58 280242.28 65422.38 280246.13	35.43 35.43 35.43 11 35.43 35.43 35.43 11	Direct		5 117.65	0.9 0.0723 0.06	1 0.0651 21.3	0.0651 0.0651 21.2 21.3	27.1	454.9 0.052 1.8	0.0 1 3	-	16,3.0X 213 5.8	. =		
		BC2 MH BD1 SEP	65423.87 280247.73 65489.42 279001.59	35.44 35.44 35.44 11 32.82 32.82 32.82 11	Direct		5 117.65	0.9 0.0771 0.065	4 0.0654 22.7	0.0694 0.0694 22.7 22.7	415	482.9 0.069 2.4	0.03 0.5 3	-	56,3.0X 30.6 10.9	- 861		
		BEI SEP SEP	65492.15 279040.81 654.00.55 279040.81	32.63 32.63 32.63 1	Direct		5 117.65 5 117.65	0.9 0.0582 0.05.	2 0.0524 17.1	0.0524 0.0524 17. 17.1	28	482.9 0.059 2.14	0.03 0.5 3	1	56,30X 238 4.2	A01		
		BF2 MH	6549114 279359.76	30.6 31.86 31.2			C0711	10 00100	C'IC 24110 24	CUC 010 7400 7400	2				696			
		EG1 COMBO SEP TWIN C1 SEP TWIN	65367.05 280442.53	31.26 31.26 31.26 1 36.4 35.4 36.4 1	Direct		5 117.65 5 117.65	0.9 0.089 0.06	01 0.0801 26.2 .9 0.0949 31	0.0801 0.0801 26.2 26.2 0.0949 0.0949 31 31	31	35.3 0.04.2 5675.7 0.056 1.9 ⁻	0.03 0.8 3	0.04.7 1	10,3.0X 27.6 3.4	LOST		
		Ex.J1 GULLY D1 GULLY	65368.75 280447.07 65347.56 280369.4	36.77 36.57 36.57 108 37.08 11	Direct		5 117.65	50.0 70.0 5.0	s 0.035 11.8	0.036 0.036 11.6 11.8	11.8	238.5 0.021 2.9	0.01 1.3 1	1	16,0.5X 6.7 5.1			
		02 MH E1 SEP	65353.57 280366.23 65393.2 280341.26	11 65.35 80.75 80.75 10 10 10 10 10 10 10 10 10 10 10 10 10	Direct		5 117.65	0.9 0.0723 0.06	5 0.065 21.3	0.065 0.065 21: 213	213	2012 01049 111	E 7.0 2).0	1	5G,30X 19.8 1.5	- 12		
		EX AK3 MH F1 COMB0 SEP	65380.84 280338.34 65379.58 280335.58	36.77 36.77 36.77 36.28 36.28 36.28 1	Direct		5 117.65	11.0 1051.0 0.11	1 0.1171 38.3	0.1171 0.1711 38.3 38.3	38.3	2975.7 0.061 2.1	0.04 0.9 33	-	16,3.0X 27 11.3	- 13		
		G1 SEP G2 MH	65391/73 280289.01 65391/22 280289.03	35.87 35.87 35.87 11 35.87 35.87 35.87	Direct		5 117.65	0.9 0.125 0.11	36.8	0.1125 0.1125 36.8 36.8	48.1	2995.4 0.066 2.3	0.04 0.9 3.	-	16,3.0X 29.4 18.6	881		
		H1 SEP	654.05.51 280.293.54 654.43.4 280.192.46	35.92 35.92 35.92 11 34.88 34.88 34.88 11	Direct		5 117.65 5 117.65	0.9 0.0677 0.06	19 0.0609 19.9 5 0.1186 38.8	0.0609 0.0609 19.5 19.9 0.1186 0.1186 38.3	21.4	447.4 0.047 1.6 ⁻ 454.9 0.063 2.2	0.03 1 3		1G,1.5X 15.6 5.8 1G,3.0X 28.4 16.2	BC1 K1		
		J1 COM60 SEP I2 GIII 1Y	6543692 280169.22 654398 280169.22	34.77 34.77 34.77 1	Direct		5 117.65	0.9 0.0455 0.04	1 0.041 13.4	7 61 7 61 137 137	22.7	2797.2 0.045 20 2584.7 0.057 2.0	0.02 0.9 2		16,15X 15.1 7.6 16.30X 23.9 9.3	L0ST		
		K1 SEP K2 MH	65461.39 280146.51 654.014 28014.65	11 177E 177E 177E	Direct		5 117.65	0.9 0.0514 0.04	52 0.0462 15.1	0.0462 0.0462 15.1	313	1672.8 0.055 1.9;	0.(3	-	1G,3.0X 23.5 7.8	μ		
		K3 COMBO SEP	65440.01 280138.03	1 07.15 17.15 17.16 1 07.15 17.15 17.16	Direct		5 117.65	0.9 0.0731 0.06	18 0.0658 21.5 1 0.0221 0.0	0.0658 0.0658 215 215	215	2285 0.028 2.9	0.01 1.9 0.		26.0.5X 10.5 11.1	M2 DCT		
		MI COMBOSEP TWIN	65484,27 280088.05	33.91 33.91 33.91 11	Direct		5 117.65	0.9 0.1212 0.10	10 10501 35.6	0.1091 0.1091 35.6 35.6	43.4	70.7 0.053		0.071 1	13 0.0 001/0	1021		
		M2 COMBUSEP I WIN M3 MH	65454.96 280080.13 65454.96 280079.02	79.15 17.55 17.55 79.75 17.55 17.55							28.8	1540.7 0.076 2.7	F 10 Z10	-	50,50X 28.8	LOS I		
		N1 IW N2 HW suffet	65521.81 279075.98 65522.52 279088.07	91.15 81.15 97.15 97.15 97.15 97.15							0				0	1 6		
		01 SEP R1 SEP	65498.65 280051.33 65515.67 279984.54	34.22 34.22 34.22 1 35.96 35.96 35.96 1	Direct Direct		5 117.65 5 117.65	0.9 0.084.9 0.07	54 0.0764 25 2 0.0462 15.1	0.0764 0.0764 25 25 0.0462 0.0462 15 151	25 18.9	723.5 0.04.2 1.5 1018.1 0.034 1.7	0.03 2 21		26,15X 15.5 9.5 26,15X 13.6 5.4	LOST CAUTION LOST SEPAVIFIC SHOWN ADF TO	RETISED AS A GLIDE DNI V	E E
		R2 SEP 01 SEP	65530.46 279942.86	35.24 35.24 35.24 1 36.72 36.72 36.72 1	Direct		5 117.65 5 117.65	0.9 0.1085 0.09	76 0.0976 31.9 4 0.0674 22	0.0976 0.0976 315 31.9	425	1079.4 0.051 1.8 500.9 0.046 1.6	0.05 2.4 3 0.03 1.2 3		2G,3.0X 24.7 17.7 16,3.0X 18.2 3.8	M2 SERVICES SHALL BE MAN R1 MECHANICAL EXCAVATIO	JALLY LOCATED BY HAND PRID	R TO
		0.2 SEP 0.3 MH	65516.35 279938.44 65491.73 279996.69	36.43 36.43 36.43 11 35.23 35.23 35.4	Direct		5 117.65	0.9 0.0995 0.08	36 0.0896 29.3	0.0896 0.0896 29.3 29.3	29.3	765.8 0.05 1.8	0.03 1.2 3	-	1G,1.5X 18.7 10.6	R2 DBTAINED PRIOR TO SITE SHALL BE UNDERTAKEN I	WORKS AND A DBYD ENQUIRY O EARLIER THAN 30 DAYS BEFO	ORE
		0.5 MH S1 SEP	654.69.14 279984.94 65554.08 279799.17	35.28 35.28 33 36.48 36.48 36.48 11	Direct		5 117.65	0.9 0.0942 0.084	8 0.0848 27.7	0.0848 0.0848 27.2 27.7	27.7	243 0.048 1.6	0.(3 1.6 3	-	2G,3.0X 19.1 8.6	CONSTRUCTION A FULL S BE KEPT ON SITE AT ALL U1 TO BE DELOTATED (2001)	ET DF THE DBYD DOCUMENTS AN TIMES, CONFLICTING SERVICES A CTED TO THE SATISFACTION DF	ARE TO
														-		SERVICE AUTHORITY PRI	R TO WORKS.	
		AUTHORISATION	7	APPROVED		SCALE		(A1) HE	ENLEY BF	ROOK AVE - ST	AGE 3			1	•	DRAWING No:	REV No:	
		FROJECT MANAGER	DATE	DESIGN CO-ORDINATOR	DATE	DATUM:	A.H.D.	MES	SARA AVENUE TO) PARK STREET		PROFO	RACIVIL			R771-126	0	
		DESIGNED DWEERTS	CHECKED	DATE DF	3AWN CCAYATTE			DU	AL CARRIAG	EWAY		ENGINEER	ING GROUP	X	city of cwar			
		© COPYRIGHT	THE DOVIDER OF THE DOVIDER AND THE	COTY OF SMARY THE POSTARENT MAY	DE HELD END THE DIDONE	DO DOMINIO DE DE DE	N SCHWIGHTON IN CAN DESCRIPTION	DR	AINAGE HYD	IRAULICS Q10				Z		OPER	ATIONS	
0 04.23 DW ISS REV. DATE BY DE	SUED FOR CONSTRUCTION SIGNIPTION	INDAGEMENT FOR THE COL	MISSION AS AGREED WITH THE CIT	ITY OF SWAN, UNJUTHORISED USE OF	THIS DOCUMENT IN ANY W.	AV IS PROHIBITED.	variation variation of the second seco							٢				

HYDRAULICS Q10 (10% AEP)

																																									ERVICES SHOWN ARE TO BE USED AS A GUDE DNLY SERVICES SHOWN ARE TO BE USED AS A GUDE DNLY SERVICES SHALL BE MANUALLY LICATED BY FAND PROR TO	MECHANICAL EXCAVATION RELEVANT PERMITS SHALL BE OBTAINED PRIOR TO SITE WORKS AND A DBYD ENQUIRY	SHALL BE UNDERTAKEN NO EARLIER THAN 30 DAY'S BEFORE CONSTRUCTION A FULL SET OF THE DBY'D DOCUMENTS ARE TO BE KEPT ON SITE AT ALL TIMES. CONFLICTING SERVICES ARE	TO BE RELOCATED/PROTECTED TO THE SATISFACTION OF THE SERVICE AUTHORITY PRIOR TO WORKS	DRAWING No: REV No:	R771-127 0		UPERATIONS
x Panol (Chake	Epith Factor Curve Name Flow QQ Flow QD Node (m) (-1 (-) (1/5) (1/5) (-) -	118.8	1 26,5,0X 215 3.5 L0ST		0.3 1 20.4 LOST 0.3 1 15.9 LOST	1 16,15X 0 AG1 1 0.56,30X 0 A015	1 0.56,30X 16.7 0.4 AL1	1 0.56,15X 15.5 2 BG1 1 0.56,30X 16.3 0.3 AJ1	1 056,30X 165 0.4 AK1 207 =	1 0.56,30X 16.9 0.5 4/1 1 4.6.05X 7.2 134.6 7.05T	1 2615V 130 58 A71	1 4.6,0.5X 3.6 0.9 LOST	1 26,30X 29.6 11.9 A06 1 056.30X 23 3.6 A07	1 0.56,3.00 185 0.9 A00	1 0.56,30X 15 AU9	1 0.56,3.0X 13.8 A.011 1 0.56,3.0X 13.7 A.012 1 0.55,3.0Y 13.4 A.013	1 0.56,30X 12.3 A014 1 0.56,30V 12.3 A014	2040 1 23.9	1 0.56,3.0X 17.5 0.6 AN1 0.66,3.0Y 19.6 1.4 AD1	1 46,15X 510 0.1 A03	1 46,15X 137 5.5 AS3 1 46,15X 137 5.5 AS3 1 46,10X 170 118 ACL	1 26,15X 18.8 17.1 AS6	1 2G.3.0X 26 20.6 AW1	1 26,15X 0 LOST 1 46,15X 201 10.2 LOST	1 0.56,3.0X 105 948.5 L0ST	- 1 26,3.0X 34,2 18.9 801	1 16,1,5X 19,1 3,1 L0ST 0.61 16,3,0X 215 33.2 .2	1 16,30X 213 5.8 1	1 0.56,3.0X 30.6 10.9 BE1		.04.7 1 28.2	1 16,0.5X 6.7 5.1 LOST	1 0.56,3.0X 19.8 1.5 H1	1 16,3.0X 27 11.3 61 1 16,3.0X 29,4 18,6 881	1 16,15X 15.6 5.8 BC1	1 16,3.0X 28.4 16.2 K1 1 16,1.5X 15.1 7.6 L0ST	1 10,5.0X 23.5 9.5 11 1 16,3.0X 23.5 7.8 M1	1 2G,0.5X 10.5 11.1 N2 1 1G,1.5X 6.8 1.7 LOST	1071 1 434 LOST 1 0.56.30X 288 LOST	0		1 20,30X 24.7 17.7 N2	1 10,15X 18.7 10.6 R2			Y	citvof swan	i de la comercia de la comerc
Foart Flonded Flonded Road Road Road Max	Capacity Depth Width Vel.Dep Grade Xfat Ds (./s) (m) (sq.m/s) 1%) 1%) 1%) 1%) 1%)		244.8 0.049 0.9 0.04 2.1 3011		397 0.044 397 0.038	0.8 2.6	482.9 0.04.9 1.78 0.02 0.5 3	476.7 0.052 1.9 0.02 0.4 3 1.98 0.049 1.76 0.02 0.5 3	482.9 0.04.9 1.77 0.02 0.5 3	482.9 0.04.9 1.79 0.02 0.5 3 1179.1 0.11.6 5.96 0.36 3.2 1	1112 1112 1112 1112 1112 1112 1112 111	1 6E 100 E51 7100 L874E	5535 0016 195 0.04 15 3 2716 0019 2.06 0.03 0.6 3	2216 0.012 1.00 0.02 0.5 3 2216 0.012 1.83 0.02 0.5 3 2216 0.016 1.46	215 0.048 1.65 0.02 0.5 3 2216 0.046 1.6 0.02 0.5 3	2216 0.0% 161 0.02 05 3 2216 0.0% 1.61 0.02 0.5 3 2316 0.0% 1.59 0.02 0.5 3	2216 0.044 154 0.02 0.5 3 2215 0.04 154 0.02 0.5 3 2235 0.047 154 0.02 0.5 3	0 c c.v 2000 son 2000	482.9 0.05 1.82 0.02 0.5 3 482.0 0.05 1.82 0.02 0.5 3	1589 0.02 0.89 0.01 3.9 2.3	7/73.4 0.015 1.24 0.03 3.9 2.8	2/94.8 0.014 2.73 0.03 3 15	633.5 0.055 1.92 0.05 2.1 3	0.4 0.015 0.72 0.09 4.2 2.6	337.9 0.6 5.81 0.4 0.6 3	\$45.1 0.058 2.12 0.05 2 3	6316.1 0.05 1.75 0.03 0.8 3 5109.6 0.019 2.42 0.05 0.9 3	454.9 0.052 1.82 0.03 1 3	482.5 0.069 2.49 0.03 0.5 3	E C/0 E0/0 19/7 6/0/0 6/200	15.3 0.0v2 0.0v2 0.0v3 0.0v3	238.5 0.021 2.96 0.01 1.3 1	30.5 0.049 1.72 0.02 0.7 3	2475.7 0.051 2.12 0.04 0.9 3.5 295.4 0.066 2.31 0.04 0.9 3.5	4,7,4 0,0,7 1,67 0,03 1 3	454.9 0.063 2.2 0.04 1 3 2'97.2 0.045 2.07 0.02 0.9 2.2	2/84./ 0.05/ 2.01 0.03 0.9 3 1672.8 0.055 1.92 0.03 1 3	2285 0.018 2.99 0.01 1.9 0.9 114 0.028 1.5 0.01 1.1 2	10.7 0.053 0.02 0.1 3 0		2336 0.042 1.67 0.03 2 2.6 2.167 0.03 2 2.6 2.181 0.010 1.17, 0.03 2.1 2	1(19) 0.00 1.0 0.0 2.1 3 1(19) 0.001 1.85 0.05 2.4 3 7000 0.001 1.85 0.05 2.4 3	755.8 0.05 1.83 0.03 1.2 3			PROFORMCIVIL	ENGINEERING GROUP www.pioformcivil.com	
AEP) M Partial Partial Catchment Direct Annraach	CIA CA Sum CA Qc=CIA Flow Qc Row Qcg Fow Qa Gw Qa Gw Qa C Sum Ca Fow Qa C Sum Ca Sum Ca <ths< td=""><td>8.8 0.102 0.205 67 178.8 178.8</td><td>0.003 0.003 25 25 25 25 25 00153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 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MESSARA AVE</td><td>DUAL CAF</td><td>SSICHED AND IN ACCORDANCE WITH THE TERMS OF</td></t<>	24 10.00 0.0821 0.0739 0.0739 24	5 117.65 0.9 0.0999 0.0899 0.0899 29	5 117.65 0.9 0.103 0.0927 0.0927 30	5 117.65 0.9 0.0975 0.0878 32.9905 103. 247.65 11.27 0.4 82.2567 32.9027 103.	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	US Node	23	75 0	1.92	0.23	2.09					129	2.33						1.78		2 4.4	1.76	2.16	781								76.6	or 7	121	3 18		2 09	27	2.69	2.01 1.89	1.26 0.83	1.15 2.04	0.77 0.77	64.3								╡	d 1 0	
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	adia Di Pripe	(m) (parage)	0 5	5 -0.93	7 0.065	12 0.211	0.202	0.065	0.1 0.065	9.9 1.315	9 0.05 3.4 0.035	35 0.091	4 0.04	0.02	1 1.085	1 0.034	2 0.02	9.7 0.265	0.1 0.281 8 0.304	5 0.035	2.4 0.061	570'0 E	5 0.118	0.188	2.8 0.045	0.07	8.5 0.237	1.2 0.32	12 0.155	4 0.08	570.0 7	000	9 0 119	8 0.02	0.02	15 0.045	5 0.06 + 6 3.098	5.3 0.06 4 0.145	5 0.258 .2 0	0 0	3 0.02 8 0	2000 J	7.6 0.04	0.065	5.9 0.06 6 0.286	9.1 0.207					OR	W. proforme	
	Cover Pij	ab) (m)	-0.11 9.	2.51 0.	0.7 94		-0.52 0	0.7 -91	0.7 -9	0.76 0.7 -8'	-0.01 3	0.62 -31	0.81 1.	0.95 -0	2.16 0	0.91 0	0.82 -0	0.2 (0.65 -8'	0.65 -9	0.7 30	- 10 	0.72 -9	0.43 5.	0.75 -61	0.6 -5	0.65 -91	0.45 0.65 -15	0.7 -1	0.51 115	0.7 12	0.7 59	0.67	0.95	0.7 1.	0.12 0.7 0	0.7 -5	0.7 84	0.7 -81	0.72 0.0	0 36:0	0.7 3.	0.7 83	0.7 -4-	0.7 -9	0.7 -8	0.63 -8					RO RO	N G N B	
	lode Cover	(m)	66 0 37 0.7	39 0.7	84 0.7	45 0.7	32 0.7	85 0.7 27 0.7	46 0.7 66 0.7	95 0.7	03 0.7 87 0.7	78 0.7 16 0.7	81 0.7 62 0.7	46 0.7 23 0.7	04 0.7 85 0.7	66 0.7 46 0.7	27 0.7 2 0.7	23 0.7	46 0.7 87 0.7	36 0.7	44 0.7	81 0.7	21 0.7 21 0.7	36 0.7	78 0.6 57 0.7	81 0.7 62 0.7	86 1.1 2 0.7	57 0.7 08 0.7	77 0.7	87 0.7	94 0.7	71 0.7	53 0.7	71 0.7	79 0.7	24 0.7	43 0.7 23 0.7	2 0.7 2 0.7	88 0.7 38 0.7	08 0.7 86 0.7	67 0.7 45 -2	41 -2 32 0.7 80 0	2 0.7 88 0.7	38 0.7	86 0.7 66 0.7	67 0.7					<u>م</u> ا	ш	
	Pipe DS N	(m) (n	30.49 31	29.34 32	16 17.67 30.64 31.	30.24 32 30.1 31	29.95 31. 29.68 31	30.54 31 30.08 31	30.16 31. 30.35 31	30.73 32	34.86 36 34.6 35.	32.57 33. 32.13 33	31.68 32	30.89 32	30.5 32 29.26 31	30.32 31 30.13 31	29.93 31 29.77 31	29.71 31 30.93 32	31.15 32 34.87 35	34.1 35	30.37 31 30.16 31	28.86 29	35.11 36	34.26 35. 27.48 28	32.35 33.	31.56 32 31.39 32.	29.95 31 29.95 31	35.47 36. 35.97 37.	35.4 36.	34.75 35 28 27.45	33.55 34	33.27 34 33.27 34 33.48 34	33.16 34 33.39 34	32.61 33	30.94 31. 32.92 34.	34, 22 35	35.39 36	35.16 36 33.29 34	31.82 32 31.06 32	30.76 32 30.54 31	30.24 32	29.81 31. 29.81 31. 29.72 30	33.18 34. 33.18 34. 31.62 37	31.12 32 32 32	30.6 31	30.6 31			L	GE 3			
	ode Ape		31.62	37 21.38	59 31.78 18 31.77	1. 31.57 15 31.34	21.88	IS 31.75 3 31.28	6 31.56	4 31.37	33 35.11 03 34.81	87 34.57 18 32.3	16 32.03 31 31.64	52 31.22 +6 31.87	23 31.66 04 29.42	IS 31.48 6 31.29	6 31.05	2 21.73 24 31.19	7 31.41 37 35.31	57 34.57 86 34.07	4 31.36 L 31.35	3 30.12	51 23.81	21 34.99	37 32.45 37 35.34	32 3176 53 31.6	55 21.92 16 30.2	4 35.51	89 35.5 88 36.6	22 34.9 28 2185	17 33.74	1 33.41	33.18	91 32.88 71 32.88	101 22 33.19	35.07	12 31.82 31.33	8 35.59 2 35.1	2 33.14 38 31.56	38 31.06 31.76	1 31.54	13.24 1 23.89 24.75 24.75	33.86	31.36 11 31.08	9 31.87 8 31.25	6 3).71				- STA			
	Vel US N	D/AL ULATE	316	32	31.7	919 10	312	316	JE SE	32.0	35.0	35.8	33.	32.6	32.3	316	31.2	32.2	32.4	35.5	33.0	31.	31.	29.0	33.	32.6 32.6	30.6	36.	36.3	35.0	34.	34	34.1	E E	31.5	35.55	36.	36.1	34.	32.	ane ane	32.0 31.1 31.2	34.8	32	H H	31.6			ļ	AVE	EET	0010 0	2 100
	Eapacity	[n/s]	2.47	128	1.17	137	137	1.37	159	1.18	1.6	2.57	1.79	1.79	1.26	1.26	137	137	1.77	137	2.6	2.21	3.38	2.81	137	1.37	153	137	121	131	137	137	137	137	136	2.55	235	2.33	2.3	1.55	136	1.48	2.55	6	137 2.93	0.97				X	PARK STR	WAY	AULIC
AEP)	Crit Bepth	VEI VC=U/A	52.96	2.43	1.07	0 17	1.58	0.97	0.96	2.12 0.98	0.98	0.84	0 0	0 0	0 0			0.58	101 0.63	1.04	151	162	781	147	1.1 0.9	1.03	133	1.02	0.92	0.88	101	1.04	123	164	0.84	0.84	0.9	0.9	1.37	163	1.74	186	0.81	0.93	0.98	1.68				Y BR			
00 (1%	orm Bepth	(m/s)	53.43	233	128	0	141	1.22	121 122	1.23	144	0	• •			• •		0.51	137	126 230	2.58	2.35	0	2.07	131	1.29	1.62 1.59	123 0.84	1.03	108	122	1.26	141	126	0	15	153	1.61 1.76	2.24	121	153	152	1.54	E E	12 0	151				INLE	SARA AVI		AINAG
ICS 01	II Pipe N	m/s)	24	233	0.52	0.59	0.67	0.36	0.29	2.01	0.31	0.18	0 0	0 0	0 0		0 0	0.02	0.09	0.49	126	142	0	0.34	0.57	0.37	0.79	0.46 0.12	0.33	0.29	0.45	0.49	0.78	0.5	0	0.24	0.31	0.31	103 0.85	1.18 1.31	123	11	0.21	0.33	0	151				T	ΞΨ C	3 2	5
DRAUI	/Ocap Fu	(-) VEL	0.97	1.83	0.38	0 48	97:0	0.19	0.18	0.2	0.33	0.07	0 0	0 0	0 0	0 0		0.02 0.18	0.19	0.36	0.48	0.65	0	0.12	0.42	0.23	E9:0	0.09	0.28	0.21	0.33	0.36	0.15	0.37	0	0.09	0.13	0.13 0.29	0.45	0.75	0.91	0.75	0.08	0.23	0.3	1.56			0	2			WITH THE TERMS
뇌	Capacity 0	(L/s)	393.5	203	2.cb2	157.7 96.7	96.7 3127.9	175.4	175.4	261.7	176.9	283.8 175.4	175.4 285.2	285.2 272.1	272.1 272.1	388.5	388.5 388.5	388.5 195.3	195.3	96.7	183.9 GK T	156.1	238.6	198.5	96.7	175.4	108.2 175.4	96.7 96.7	85.3 96.7	7.96	96.7 1.92	96.7 96.7	96.8 61.2	96.7	216.4	180.4	156.4	164.9	162.8 319.6	241.1	291.5 610	610 652.1 7.31.6	180.6	96.7 96.7	96.7 206.9	68.4							N ACCORDANCE
	cess Pipe	(L/S)	378.6	354.9	613																																				132	385	0.00			5.7				ЦН	5		ISSIONED AND I
	Pipe Ex	(L/s)	3815 3711	370.9	37.1	6.59	0771	33.5	31.9 32.7	34.6	34.1	20	• •	0 0	• •	• •	• •	6.4 35.9	37.6 6.1	34.8	88.9	100.7	8171	24.1 84	40.5	40.7	68 87.6	32.5 8.3	23.5	20.2	31.6 31.6	34.9	55.3	35.3	0	17	21.6	21.7 41.8	72.8 134.7	187 209	266.5	510.8 4.86.7 4.70.5	14.8	23.7	29	106.8				A			ICHIT WAS COM
	Net Bypass	(L/s)	-18 q	-18.9	6 RL -			3.2	2.4	41	-3262	-3289.1	-3376.9 -3371.8	-3361	-334.0.4	-3329.2 -3325.1	-3320.3 -3324.8	-3268.2 5.4,	-33	-48 S	111-	-93.1	-114.2	-2148.1	-45.6 -18.6	-0.6 7.8	07	-24	-15.2	-16	72	7.4	-25.7	-29.6	-28.6	- 10.6	-18.5 -513	-28.8 -84	-152.6 -160.2	-160.9 -191.1	-176.2 -60.3	-603	-315	-13.2	6.0-	45.8			SCALE	NUTLE			IRPOSE FOR MHI AY WAY IS PROHI
	Peak Flow Draf	(L/S)	381.5	389.8	37.1	6.cg	0771	30.3	30	30.4	3321.2 3317	3309.1 3288.4	3306.3 3307.8	3303.8 3302.7	3291.9 3286.2	3280.6 3274.8	3268.3 3262.9	3274.6 30.4	30.7	34.8	160.3 195.6	193.8	0	2232.1	86.1	413 312	68 68	56.5 21.4	38.7	36.2	24.4	27.5	81	64.9	0	275	40.1	50.5 125.8	225.4	348 400.1	529.6	21/2	6.700 6.84	317 35.2	29.9	61					DATE	N CCAYATTE	ISED FOR THE PL DOCUMENT IN AV
	Direct Node	(5/-)					07%																																												TOR	DRAW	UMENT MAY BE L
	Part-area	(L/s)	149.8	244.6	37.1	65.3		30.3	30	30.4	1673.2	1676.9 1678.3	1729.5	1765.4	1779.6 1786.2	1792.3	1801 1806.2	1843.1 30.4	30.7	34.8	160.3 105.6	193.8	957	55.2 629.8	85.1	413 312	89 89	56.5 21.4	38.7	36.2	24.4	27.5	81	64.9	45.5	27.5 84.5	40.1	50.5 125.8	225.4	348 400.1	442.7 529.6	5/7.1 5/7.1	10.28	317 35.2	29.9	51			SOVED		N CO-ORDINA		SWAN. THE DOC VA. UNMUTHORIS
	Part-area	(ha)	0.2517	0.9915	0.0523	0.1097		0.0509	0.0196	0.0511	2.8715	3.0457	3.1727 3.2871	3.3876 3.4823	3.5748 3.6681	3.761 3.8525	3.9398 4.0312	4.184.4	0.0515	0.0585	0.281	6755.0	0.4104	0.0927	0.1447	0.0524	0.114.2	9E0'0 6760'0	0.065	0.0509	0.041	0.0462	0.1381	0.1091	0.0764	0.0462	0.0574	0.0348	0.3992	0.7371	0.8207	555	0.0778	0.0533	0.0503	0.1025			Appr		DESIG	DATE	OF THE CITY OF THE CITY OF SW
	Part-area	(mm/hr)	214.27	8832	214.27	214.27		214.27	214.27	214.27	214.27 210.8	20809 19838	19625 19203	187,61	179.22 175.3	17156 16799	164.57	15857 214.27	214.27	214.27	20534	194.6	76761	214.27	214.27 214.27	214.27 214.27	214.27	214.27	214.27	214.27	214.27	214.27	214.27	214.27	214.27	214.27	214.27	214.27 214.27	20328	201.3	194,19	17742 17742	214.27	214.27	214.27	214.27					DATE	CKED	A THE PRIPERIT
	Part-area	(vim)	s 2	24.23	5 24.28	~		s 5	s s	5	5.11	5.38	6.15 6.46	6.79	7.79	8.72 8.45	8.79 9.72	9.11	5 U	5	555	9 14 9	ò		ۍ <u>ه</u>		5 V				-		192 ur	523	5	· · ·			5.69 6.08	5.89	6.31 6.55	7.61	e		5	ŝ			NO	2	H I	ERTS CHE	A NOISSIMMOO 3
	a Full-trea	(L/S)	38:5	38:86	17582	655		303	36	304	3321.2 3317	3309.1 3283.4	3305.3 3307.8	3303.8	3291.9	3283.6 3274.8	3263.3	3274.6 304	307	348	159	1919	5353	22221	861 403	413 312	68 477	565 214	387	362	244	275	809	649	455	275	401	505 125.8	224.5 29:14	347.9	435.4 511.6	5351	1,28	317 352	299	19			THORISAT		JECT MANAGE	GNED D.WE	PYRIGHT DOCUMENT IS // GEMENT FOR TH
	ea Full-are	r) (Fa)	7.7383	7.8305	C058./ 7	6		7 0.0509	7 0.0505	7 0.0511	13.2797	13.4696	13.7412	2 14.(508	14.1367	14.129	14,599	7 0.0511	7 0.0515	7 0.0585	3 0.2338	0.3577	0/110	7 0.0927	7 0.0578	7 0.0524	7 0.114.2	7 0.034.9	7 0.65	7 0.0509	7 0.441	0.0,62	0.1381	1901.0 7	10.0164	7 0.0162	7 0.0574	7 0.0348	3 0.4013 9 0.5398	4 0.55 9 0.7616	8 0.8547 9 1.C33	177 177	7 0.078	7 0.0533	7 0.0503	7 0.1)25			ALL	2	ON	DES	NG HIS
	area Full-ar	- (um/h	93 1.82 99 1.82	21 1.81	214.2	787		211.2	211.2	211:2	21 8130	38 88.44 32 81.95	17 85.62 47 85.94	79 85.22 37 84.62	46 83.75 79 83.1	13 82.42	13 80.40	211.2	214.2	211-2	3 2016 5 10: 0	19119	0.181	72 2:56	214.2	211.2	211.2	214.2	211.2	211.2	211.2	214.2	211.2	211.2	24.2	21:2	211.2	211.2	1 2014	3 191.04	2 183.3 6 183.3	2 163.3 2 163.3 7 146.3	211.2	211.2	211.2	211.2							
	Pipe Full-	(1 in) (mi	52.6 253	197.4 254	100 25	100 5.1	330	100 5	100 5	100 5	98.3 2/ 100 24.	38.2 24. 100 25.	100 25. 100 25.	100 25. 250 26.	250 26.1 250 26.2	250 27.	250 27. 250 28.	250 28J 80.6 5	80.7 5 29.3 5	100 5 29 9 5 3	27.7 51 27.7 51	38.4 6.3	16.4 b./	23.8 5	100 5	100 5	100 5	100 5	128.5 5	100	100	100	100 5.2	100 5.2	173.8	28.7 5	33.8 5 33.8 5 5.1 5.1	34.4 5	35.3 5.8 79.7 6.1	133.2 6.5 139.9 6.8	217.8 7.1	291.7 8.4 291.7 8.4 666.6 8.6	28.7 5 28.7 5	100 5 5	100 5 21.9	200 5							
	at Grade	AT UFADE	0 19	0.51		1 1	0.3		:	1 0.56	1.02	2.62		9 1 5 0.4	5 0.4	3 0.4	3 0.4	3 0.4	1.24	1 1	1 361	1 2.6	1 6.08	1 4.21			1 1.25		1 0.78				1 1		9 0.58	1 3.48	1 2.96	1 2.91	1 2.83 9 1.26	9 0.75	5 0.46 2 0.3	2 0.34 2 0.34	1 3.48		1 1	1 0.5							
	Full P	(sq.n	0.15	0.15	0.0	0.07	0.07 0.07	0.07	0.1	0.11	0.1	E 0	0.15	0.15	0.21	0.21	0.28	0.28	0.11	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.07	0.15	0.07	0.07	0.07	0.07	0.15	0.21	0.44	0.07	0.07	0.07	0.01							
	IE Pipe	1 (mm)	22 450	2 450	157 151	33 300	71 300 21 (3x)x6-	79 375 300 300	72 375	1 (2x)3 375	375 375	27 375 51 375	55 450	32 450	0 525 1 525	525	75 600	3 600 12 375	85 375 '8 300	53 300	8 300	52 300	300	47 300	53 300	65 375 75 300	1 375	1 300	300 300	300	300 300	300 300	300	24 300	12 450	35 300	37 300	52 300	94 300 11 450	1 450	99 525 75 750	15 750 7 750	5 300	5 300 36 300	7 300	75 300							TRUCTION
	did ad d	(-) (m.	CP 4 6.6	CP 4 6.7	CP 4 72.5	CP 4 23.	RCB 4 25. RCB 66.1	CP 4 20.	CP 4 20.	CP 4 35.	CP 4 25.	CP 4 75.	7.6E 7 dD	CP 4 33.	CP 4 40	07 7 dD	CP 4 34.7	CP 4 20.6	CP 4 20.0 CP 4 12.8	157 7 d	10 4 54	CP 4 48.0	CD 7 312	CP 4 23.4	101 7 101 13.4	CP 4 20.1 CP 4 20.7	PE SN8 8 CP 4 235	CP 4 6.9	CP 4 121	10 4 14.4	CP 4 195	CP 4 13.5	CP 4 19	CP 4 271	PE SNB 12.1 CP 4 26.4	CP 4 24	CP 4 63 2	CP 4 14.1 CP 4 82.6	CP 4 39.5	CP 4 30	CP 4 28.	CP 4 76.	CP 4 19.	CP 4 26.3	CP-4 27.	31 to 53							ED FOR CONS TRIPTION
	adi	~	0 AB2 R	8 198 P.	0 AD2 R	to S10 R	to S11 F	o AG11 F	o A013 H	o AM2 k	o A02 F	e A04 F	to A05 F	e A09 F	o A010 F	o A012 F	to A014 F	to A016 R. o A09 R.	Po AOB R	O AS2 R	A 454 P	0 AS6 R	O ATZ R	o AW2 R	o AO4 F	o AO5 F	• BF2 HD. • A015 R.	o D2 R	EX Ak3 R	0.051 R	0 J2 R	o K2 R	Ex A01 R	o M2 R	o N2 HD: x A03 R	0 R2 R	0 D2 R	0 S2 R	10 S4 F	to S6 F	to S8 F	10 S10 F	0 S3 R	0 S6 R	10 S7 R	10 S8 R							3 DW ISSL
	ď	-	AB11 AB2 +-	AB3 1.	AD1 F.	AD2 AF1 +	AG1 AH1 h.	AI1 to AJ1 to	AK1+ AL1+c	AN1 Hc	A01 F A02 F	A04 F	A05 1 A06 h	A07 1 A08 †	A010 †	A011 F A012 ±	A013 1 A014 h	A015 1 AP1 h	A011 AR1 ht	AS11 AS2+	423 t	455 +	ATT	AT2 1 AW1 h	AZ1 + B1 to	BE1 tc	BF11 BG11c	C1 10 D1 h	E1 to L	Ē	110	K1F K1F	K3 to	M1 F	N1 F	R1 F R2 ±	01+	S1 F	S4 † S4 †	S6 h	S7 S8 +	S101 S101	10	W11 X1 ft	711 Z1 h	22 1							0 04.2 BEV DATE

BEFORE J DIG 00.com.au	

		Nacip Varip	Setaut	Setaut Setaut Gra	te Caver Catch	Tc Catch	Catch Catch T	HYDROL Intensity Runaff		1% AEP)	ial Partial Partial	Catchment Dire	+ Annraeri R	Flooded Flo	oded Flocded Ros	d Road Max Pond	Chake Inlet	Intet Bynass By	Ster	VOU D	S C R
		Name [ype (-)	Easting (m)	Varthing RL RL (m) (m) (m)	RL ID (m) (-)	Method Length (-) [m]	Slope Retardance (x) (r	c I C n) (mm/hr) [-)	A CA (ha) lha)	Sum CA Qc=CIA Ci (ha) (L/s) (hi	A Sum CA Qc=fIA (ha) (L/s)	Flow Gc Flow	rcg Flow Qiz Cal	acity Depth N	dth VelDep Gra	de Xfall Depth (%) (%)	Factor Curve Nam (-) [-)	E Flow 3g Flow 0b N	-	WWW.1100.co	no.mo
		A1 SEP A2 MH	65368.86 2	80499.42 36.16 36. 80507.61 36.16 36.	16 36.16 16 36.06								0					0			
		AB1 HW	65486.16 2	79492,43 30.62 316	3 3163 1	Direct 700 ro		214.27 0.9	0.1133 0.102	7.7083 381.5 0.1	02 0.2517 1498	381.5	381.5					381.5	ī		
		AB2 GULLY	65492.2 2	19489.75 31.66 31.6	i6 31.66 11 K	Direct 290.59	0.5 0.25 25	.93 17.82 0.45 214.27 0.9	16.9029 7.6063 0.068 0.0612	0.1722 4.2.7 0.06	98 12 0.0843 50?	50.2	50.2 2	4.8 0.056 0	93 0.07 2.	301.1	0.8 2G,5.0X	31.3 18.9 L	0ST		
		HM VB3	65514.09 2	79474.46 32.37 32.	37 32.37 3P K	nematic Wave 100	2.5 0.25	6 89.36 0.45	0.2465 0.111	0.0	8								7		
		A84 MH A85 CULLY	65544.37 2	79468:57 32.39 32. 79418.43 31.54 31.5	39 32.39 44 30.55														ē 1		
		A01 GULLY A02 GULLY	65570.94 2	79473.87 31.78 31.7 79473.87 31.84 31.8	11 31.78 11	Direct Direct		214.27 0.9	0.0542 0.0623	0.0623 37.1 0.06	23 00623 371 87 00487 29	37.1 29	37.1 1 29 1	88.5 0.092 88.5 0.079		0.3	0.5	37.1 L	0ST 0ST		
		AFT SEP Act SEP	65537.14 20030 73	279398.8 31.35 31.35	5 31.35										00	2.6	0.8 16,15X	0	G1		
		AH1 HW Triple AH2 HW nitlet Triple	65472.95 2 65472.95 2	79356.4.3 29.68 33 79356.4.3 29.68 33	7. 30.88 7. 30.68							571	1440					1440			
		All SEP	65502.9	79200.58 31.85 31.8	5 31.85 1	Direct		214.27 0.9	0.0566 0.0509	0.0509 30.3 0.05	09 0 0 5 09 30.3	30.3	731 4	32.9 0.085 3	07 0.45 0.5		0.8 0.56,3.0X	33.5 39.5	11		
		AVI SEP	65508.83 2	79280.22 31.47 31.4 102.002 31.47 31.4	7 31.0 1	Direct		214.27 0.9	0.0551 0.0496	0.0496 29.5 0.04	24 0.0524 31.2 96 0.0496 29.5 or ocror 30	31.4 29.5 3.6	1.00	15.7 U.000 3 98 0.082 2	10 110 010 010 010 010 010 010 010 010	n m r	0.8 0.56,30X	31.5 34.5	101		
		AM1 HW Double	6549363	719181,58 30,37 31,1 719181,58 30,37 31,1 7046 75 75 75 75 75 75 75 75 75 75 75 75 75	4 3114 3P K	nematic Wave 597.18	0.4 0.25 22	3.3 19.1 0.45	18.6082 8.3737	8.3737 444.2 8.37	37 8,3737 444,2	2.444	7.444	r			Variana	5 ac 2.444			
		AN1 SEP	67:00:559	79160.43 32.05 32.0	25 32.05 11	Direct		214.27 0.9	0.0568 0.0511	0.0511 30.4 0.0	511 0.0511 30.4	30.4	77.3 4	32.9 0.087 3	14 0.05 0.5		0.8 0.5G,3.0X	34.6 428			
		AUT CULLT	0110400	0100 00100 07160001	= 0.00 0	nematic Wave 100	2.5 0.25	57:0 9:17	29.6648 13.3492	2.78	75101 711017 CA	71700	1 71766	D /CI/A /2/	FIC 70:0 40	-	VC:0'D4 0'0	7 7076 7:46	101		
		A02 SEP A03 SEP	65482.53	78859.15 36.03 36.0 78874.71 35.87 35.8	33 36.03 11 37 35.87 11	Direct Direct		214.27 0.9	0.0151 0.0136	0.0603 35.9 0.06 0.0136 8.1 0.01	03 00603 35.3 36 0.0136 8.1	35.9 8.1	35.9 14 30	75.2 0.04 2 48.7 0.02	17 0.03 2. 2 0.01 3.5	19	0.8 26,15X 0.8 4G,05X	5.3 5.2 L	21 35T		
		A04 A05 SE ² TWIN	65496.55 2	78950.97 33.78 33. 78964.22 33.16 33	18 33.78 16 33.16 11	Direct		214.27 0.9	0.14.11 0.127	0.127 75.6 0.1	27 0.127 75.5	75.6	75.6 5	53.5 0.07 2	51 900 77	8	0.8 2G,3.0X	33.3 42.2	- 05		
		A06 SEP A07 SEP	65509.37 65512.51 2	279000.2 32.81 32. 79039.32 32.62 32.6	31 32.81 11 52 32.62 11	Direct Direct		214.27 0.9	0.05 0.0481 0.0534 0.0481	0.04.91 28.6 0.0	45 0.045 26.3 81 0.0481 28.5	26.8 28.6	69 3	21.6 0.084 2 21.6 0.082 2	95 0.45 0.6 88 0.45 0.5	m <i>m</i>	0.8 0.5G,3.0X 0.8 0.5G,3.0X	32.6 36.5 J 31.6 33.5 J	07 08		
		A08 SEP	65514.42 2	79072.59 32.46 32.4	6 3246 11	Direct Direct		214.27 0.9	0.048 0.0432	0.0432 25.7 0.04	32 00432 251 11 00111 21 5	25.7	59.2 3	215 0.08 2	78 0.41 0.5		0.8 0.50,30X	30.1 29.1 /	03		
		A010 SEP	71702529	79159.06 32.04 32.0	04 32.04 11	Direct		214.27 0.9	0.0469 0.0422	0.0422 25.1 0.04	22 0.04.22 25.1	25.1	5 7:05	21.6 0.075 2	62 0.44 0.		0.8 0.56,30X	213 231 1	110		
		A011 SEP AC12 SEP	65523.22 2	79238.87 31.65 31.8 79238.87 31.66 31.6	6 31.65 11 6 31.66 11	Direct Direct		214.27 0.9	0.0455 0.042	0.042 25 0.0	42 0.042 25 41 0.041 24.4	25 24.4	48.1 3 45.9 3	21.6 0.074 2 21.6 0.072 2	57 0.44 0.5		0.8 0.5G,3.0X 0.8 0.5G,3.0X	25.9 20 /	013		
		AC13 SEP AC14 SEP	65529.22 2 65531.56 2	79278.74 31.46 31.4 79318.67 31.27 31.2	6 3146 11 17 3127 11	Direct Direct		214.27 0.9	0.0433 0.039 0.0433 0.039	0.0377 22.4 0.0	77 0.0377 22. 39 0.039 232	22.4	42.4 3	21.6 0.07 2 33.5 0.073 2	46 0.03 0.5 54 0.03 0.5	<i>m</i> m	0.8 0.56,30X 0.8 0.56,30X	24.8 17.7 A 24.3 16.6 A	314 015		
		ACIS COMBOSEP TWIN ACI6 HW putter	65533.97 2	79353.34 31.2 31. 79355.93 29.7 31	2 312 11	Direct		214.27 0.9	0.0812 0.0731	0.0731 4.3.5 0.0'	31 0.0731 4.3.5	43.5	60.1	8.4 0.09		0.045	0.5	60.1	7 5		
		AP1 SEP	65497.7	279120.4 32.24 32.2	24 32.24 11	Direct		214.27 0.9	0.0568 0.0511	0.0511 30.4 0.0	102 10211 30.4	30.4	82.8 4	32.9 0.089 3	22 0.45 0.5		0.8 0.5G,3.0X	35.9 46.9	LN .		
		AR1 SEP AR1 CULLY	65497.64 2	79074.03 32.47 32.4 78862.01 36.37 36	37 36.37 11	Direct		214.27 0.9	0.0572 0.0159	0.0159 50.7 0.01	(15 0.0515 30.7 59 0.0159 9.5	30.7 9.5	90 4	58.9 0.092 3 58.9 0.025 1	32 0.05 0.5 11 0.02 3.5	23	0.8 0.50,30X 0.8 46,15X	57.6 52.4 6.1 3.3	C3		
		AS1 CULLY AS2 CULLY	65468.1 2	78921.88 35.57 35. 78789.94 35.36 35.	57 35.57 11 36 35.36 11	Direct		214.27 0.9	0.065 0.0585 0.0588	0.0585 34.8 0.05	85 0.0585 34.3 88 0.0588 35	34.8 35	34.8 35 70	1 E70'0 7'EL	55 0.05 3.5	2.8	0.8 46,1.5X	34.8 17.4 /	- ES		
		AS3 SEP AS4 SEP	65515.67 2 6554156 2	181 24 24 25 25 25 25 25 25 25 25 25 25 25 25 25	1 33.54 1	Direct		214.27 0.9	0.0819 0.0737	0.0737 4.3.9 0.07	37 0.0737 4.33 39 0.0739 4.4	43.9	613 843 25	278 0.054 1 34.8 0.054 1	96 0.05 3. 75 0.04 3	3.1	0.8 4.6,3.0X 0.8 26.15X	21 40.3 1	S4 S6		
		ASS MAL	65555.9 2	78689.43 31.3 31.	3 313	1110		00 10 100				100	440 C] ^	AVE 34 6.0		3 - 17		
		ASO GULY TWIN	65602.37	78644.4 28.76 28.	1 29.01	UILECT		6.0 17:417	4400.0 4440.0	20.0 0.00 4400.0	C.CC 4400.0 44	0.50	0	///// 0.00	7 64.0 /	n -	¥6'5'07 5'0	1 1 60 7 76	I M		
		AT1 SEP A-2 GULLY	65534.28	778827.3 37.6 37. 78802.33 36.21 36.	6 37.6 21 36.21 11	Direct		214.27 0.9	0.103 0.0927	0.0927 55.2 0.05	27 0.0927 552	55.2	55.2	0 2002 0	72 0.16 4.2	3 26	0.8 ZG,15X 0.8 4.G,15X	0 24.1 311 L	0ST DST		
		AW1 SEP	65615.78 2	78597.47 29.05 29.0	35 29.05 11 3P K	Direct nematic Wave 624.5	0.6 0.25 19	72 214.27 0.9	0.0975 0.0878 82.2567 37.0155	37.1033 2232.1 0.08	78 1.0582 6298 04 04	2232.	2315.2 3	37.9 0.15 5	81 0.88 0.6	m	0.8 0.5G,3.0X	84 22312 L	ISI		
		AW2 CULLY AZ1 SE2 TWIN	62639.59	278596.7 28.15 28. 78951.69 33.37 33	IS 28.15 37 33.37 11	Direct		214.27 0.9	0.1507 0.1447	0.1447 86.1 0.14	47 0.1447 86.1	86.1	107 9	45.1 0.076 2	75 0.08 2		0.8 26.3.0X	40.5 66.5	- 10		
		BI SC TWIN	65381.4.4 2	80449.66 36.37 36	36.37 11	Direct		214.27 0.9	0.0753 0.0678	0.0678 40.3 0.00	78 0.0578 4.0.3	40.3	6.04	16.1 0.063 2	19 0.64 0.8		0.8 10,1.5X	21.7 18.6 L	05T		
		BC1 CUMBU SEP	65422.38	80246.13 35.43 35.4	3 35.43 1	Direct		214.27 0.9	0.0723 0.0651	0.0 7.60 2011.0	1.co 0.0651 38.7	38.7	70 4	160.0 9.60	56 0.05 1	n m 4	0.3 16,3.0X	28.8 412	1		
		B01 SEP B61 SEP	65489.42 65492.15	79001.59 32.82 32.8 7904.0.81 32.63 32.6	32 32.63 11 53 32.63 11	Direct Direct		214.27 0.9	0.0771 0.0694 0.0524	0.0524 41.3 0.06	94 00694 413 24 00524 312	413 312	107.8 4 98.2 4	32.9 0.098 3 32.9 0.095 3	43 0.46 0.5 43 0.46 0.5	m m	0.8 0.50,30X 0.8 0.50,3.0X	38.9 59.3	01		
		BF1 COMB0 SEP TWIN	65490.55 2	79367.73 30.65 30.6 7934.7.43 31.26 31.2	55 30.65 11 56 31.26 11	Direct		214.27 0.9	0.1269 0.1142 0.089 0.0801	0.1142 68 0.11 0.08 0.11	42 0.1142 68	68 47.7	68 87.6	7.6 0.123		L70'0	0.5	68 87.6	5 7		
		CI SEPTWIN	65367.05 2 65367.05 2	8044253 36.4 36. 8014707 36.77 36	4 36.4 1	Direct		214.27 0.9	0.1055 0.094.9	0.0919 56.5 0.05	49 0.0949 56.5	56.5	56.5 56	75.7 0.071 2	46 0.05 0.8	<i>n</i>	0.8 1G,3.0X	32.5 24 L	IST		
			6534756	280369.4 37.08 37.0	10 2020 10	Direct		214.27 0.9	9E0:0 70:0	0.036 21.4 0.0	*12 9E0.0 9E	21.4	21.4 2	38.5 0.027 3	69 0.31 1.3	-	0.8 1G,0.5X	8.3 13.1 L	- 05T		
		E1 SEP	65353.57 2	80366.23 37.08 37.0 80341.26 36.39 36.3	36.39 11 36.39 11	Direct		214.27 0.9	0.0723 0.065	0.065 38.7 0.0	55 0.065 38.7	38.7	38.7 3	30.5 0.062 2	16 0.44 0.7	8	0.8 0.5G,3.0X	23.5 15.2	1 2		
		EX Ak3 MH	65380.84 2	80338.34 36.77 36.7 80335.58 36.78 36.7	77 36.77 38 36.78 11	Dirart		20 1C 71	0.1301 0.1171	10 101 101	103 1011 10	7.03	50.7 20	75.7 0.07K 2	AC 0.05 0.0	35	0.8 16.2AV	132 217	1 5		
		EI CUMBUSEP	00:61000	80289.01 35.87 35.8	1 35.87 11	Direct		214.27 0.9	0.125 0.1125	0.1125 67 0.11	25 0.1125 67	1.40	102.4 29	95.4 0.087 3	50 L00 90	35	0.8 1G,3.0X	34,8 67,6	81		
		H1 SEP	65443.4 2	80293.54 35.92 35.9 80192.46 34.88 34.3	22 35.92 11 38 34.88 11	Direct Direct		214.27 0.9	0.0677 0.0609 0.1318 0.1186	0.0609 36.2 0.06 0.1186 70.6 0.11	09 0 06 09 36.2 86 0.1186 70.5	36.2 70.6	515 4	47.4 0.066 2 54.9 0.089 2	32 0.04 1	e e	0.8 1G,1.5X 0.8 1G,3.0X	20.2 31.2 36.3 75.5	41		
		J1 CONBO SEP	65436.92 654.30 R	80169.22 34.77 34.	11 34.77 11	Direct		214.27 0.9	0.0455 0.041	0.041 24.4 0.0	41 0.041 24.1	24.4	88.4 27	97.2 0.075 3	45 0.45 0.5	22	0.8 1G,1.5X	316 56.8 L	1		
		K1 SEP	65461.39	80146.51 34.41 34.	11 34,41 11	Direct		214.27 0.9	0.0514 0.0462	0.0462 27.5 0.04	62 0.0462 27.5	27.5	103 16	72.8 0.086 3	01 0.07 1		0.8 1G,3.0X	34.9 68.1	5		
		K3 CONBO SEP	65440.01	80138.03 34.71 34. 80138.03 34.39 34.	34.39 11	Direct		214.27 0.9	0.0731 0.0658	0.0658 39.2 0.06	58 0.0658 39.2	39.2	39.2 2	285 0.035 3	74 0.02 1.5	0.9	0.8 2G,0.5X	12.6 26.6	12		
		L1 CULLY MH	654,38,19 2	80137.28 34.53 34.7 280128 34.44 34.4	53 34.53 44 11	Direct		214.27 0.9	0.029 0.0261	0.0261 15.5 0.03	61 0.0261 15.5	15.5	15.5	14 0.035 1	88 0.42 1:1	2	0.8 1G,1.5X	9.1 6.5 L			
		M1 COMBC SEP TWIN M2 COMBC SEP TWIN	654584.27 2	80088.05 33.91 33. 80080.13 33.71 33.	91 33.91 11	Direct		214.27 0.9	0.1212 0.1091	0.1091 64.9 0.10	6.1091 64.9	6.43	88.5 15	5.3 0.071 40.7 0.118 5	14 0.64 0.	3 0.071	0.5 0.5G,3.0X	35.3 97.7 L 68.5 20 L	DST DST		
		HM HM HM	65454.96 2	80079.02 33.71 33. 79075.98 31 31.5	71 33.97								0					0	1 1		
		NZ Hhv outlet 01 SEP	65522.52 2	79088.07 30.93 31.7 80051.33 34.22 34.2	9 31.79 22 34.22 11	Direct		214.27 0.9	0.0849 0.0764	0.0754 45.5 0.07	64 0.0764 45.5	45.5	45.5 7	23.6 0.053 2	08 0.64 2	2.6	0.8 26,15X	16.5 28.6 L	- 35T		
		Ex A03 CULLY R1 SEP	6547383 2 65515.67 2	80042.04 34.04 34.0 79984.54 35.96 35.9	11 34.04 11	Direct		214.27 0.9	0.0514 0.0462	0.0462 27.5 0.04	62 0.04.62 27.5	27.5	97	18.1 0.047 2	43 0.04 2	2	0.8 2G,15X	17 29 L			
		R2 SEP	62494.91 2	79997.78 35.24 35.7	24 35.24 11 m 35.77 1	Direct		214.27 0.9	0.1085 0.0976	0.0976 58.1 0.05	76 0.0976 581	581	90.9 10	79.4 0.068 2	47 0.07 21	<i>m</i> •	0.8 26,3.0X	28.9 62 24.2 18.5	12		
		02 SEP	65516.35 2	1/9E E7/9E 7/7/8E66L	1 270.02	Direct		214.27 0.9	0.0995 0.0896	0.0896 53.3 0.08	96 0.0896 53.3	53.3	53.3	10.9 U.053 2	29 0.65 1.2	0.00	0.8 16,1.5X	20.5 32.8	12		
		C3 MH SEP	65554.08	19996.69 35.25 35.46 36.4 1.05 36.48 36.4	23 35.4 11 -8 36.48 11	Direct		214.27 0.9	0.0942 0.0848	0.0848 50.5 0.05	48 0.0848 50.5	50.5	50.5	43 0.05	1 0.05 1.6		0.3 2G,3.0X	21.7 28.8	CAUTION		
		S2 SEP S3 SEP	65539.12 2	79798.78 36.2 36. 79716.16 34.2 34.	2 36.2 11	Direct Direct		214.27 0.9	0.14.29 0.1286 0.1223 0.11	0.1286 76.6 0.12 0.11 65.5 0.	86 0.1286 76.5 1 0.11 65.5	76.6 65.5	76.6 8 120.7 12	36.4 0.069 2 44.6 0.072 :	48 0.06 1.5 6 0.09 3.2	m m	0.8 2G,15X 0.8 4.G,3.0X	21.3 55.2 28.4 92.3	SERVICES SHOWN ARE TO I	E USED AS A GUIDE DNLY.	ng TO
		S4 CONBO SEP	65532.83 2	79669.34 32.88 32.8 796.99.52 32.88 32.8	38 32.88 11 38 32.38 11	Direct		214.27 0.9	0.0739 0.0665	0.0655 39.6 0.06	65 0 0 6 6 5 3 9 3 40 0 0 6 6 5 3 3 3 3	39.6	131.9 5	42.7 0.082 2 36.8 0.091 3	31 0.17 0.7	~ ~	0.8 26,3.0X	55.6 76.3 712 64	MECHANICAL EXCAVATION CC DBTAINED PRIOR TO SITE V	RELEVANT PERMITS SHALL E DRKS AND A DRYD FNQUIRY	36
		SS SEP 51	65527.38 2 65527.38	79589.62 32.08 32.0 70550.71 31.86 315	08 32.08 11 6 31.06 11	Direct		214.27 0.9	0.0583 0.0524	0.0524 312 0.05	24 0.0524 312 29 0.01.29 25.5	31.2	100.2 5	36.8 0.088 3	19 0.05 0	. m n	0.29 0.56.30X	14.2 86	CONSTRUCTION. A FULL SE	EARLIER THAN 30 DAYS BEF OF THE DBYD DOCUMENTS /	FORE ARE TO
		SI COMBOSEP TWIN	65523.01 2 65523.01 2 65516.49 2	102 57 CE 57 USCCCC	11 1916 1	Direct		214.27 0.9	0.0842 0.0757	0.0757 45.1 0.07	57 0.0757 45.1	45.1	115.2 1	115 0.134	11.0 70	0.15	VARTACIA 510	115.2	T D BE REPT ON SITE AT ALL T T D BE RELOCATED/PROTEC	MES. CONFLICTING SERVICES TED TO THE SATISFACTION D TO WORKS	DF THE
		ALITHORISAT	NOI	APPROVE		SCALE	-	_	(A1)			- HO			_	/				DEVINO	
						DATUN	AHD		HE			- SIAG	S L						D771_170		
DMEN		FROJECT MANAG	ER DATE	DESIGN CO-01	RDINATOR DA	E			MESSA		AKK STREET		<u>-</u>	ROFO	RMCIV	// =	X	,	71 <u>- 1</u> / / VI	>	
VBMA		DESIGNED D.WE	ERTS CHECKED	DATE	DRAWN	CCAYATTE			DUAL	CARRIAGE	VAT		ш	N G I N E E F	ING GRO		A city	/ Of swan			
0 04.23 DW ISSUED 1	OR CONSTRUCTION	C COPTRIGHT THIS DOCUMENT IS N	ND SHALL REMAIN THE PROF	ERTY OF THE CITY OF SWAN. T	HE DOCUMENT MAY BE USE	DEOR THE PURPOSE FOR MH	CHIT WAS COMMISSIONED AND	LACCORDANCE WITH THE TE	BOF DRAI	AGE HYDR	DLOGY Q100	0				グ	Ŧ		NT L L L L L	VIIOINO	
REV. DATE BY DESCRI	NOILC	CRUCKOCONETAN 1 AN 111	E COMMISSION NO MONITO	WITH THE CIT OF ONLY ON THE	THORSED USE OF TIRK VV	UMENT IN MIT WAT IS FINAN	100						_								